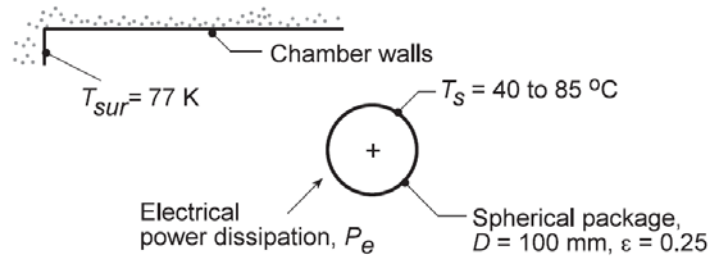


## PROBLEM 1.25

**KNOWN:** Spherical shaped instrumentation package with prescribed surface emissivity within a large space-simulation chamber having walls at 77 K.

**FIND:** Acceptable power dissipation for operating the package surface temperature in the range  $T_s = 40$  to  $85^\circ\text{C}$ . Show graphically the effect of emissivity variations for 0.2 and 0.3.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Uniform surface temperature, (2) Chamber walls are large compared to the spherical package, and (3) Steady-state conditions.

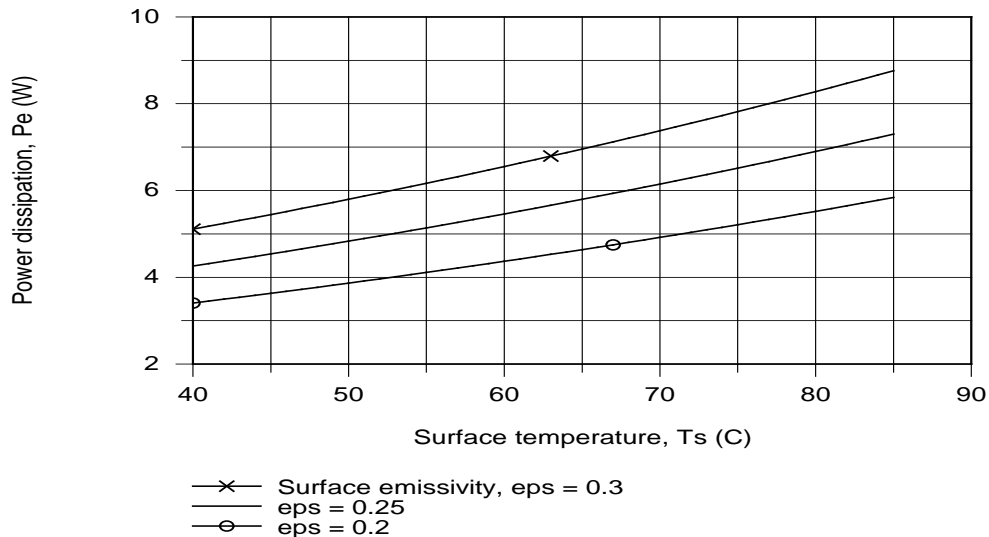
**ANALYSIS:** From an overall energy balance on the package, the internal power dissipation  $P_e$  will be transferred by radiation exchange between the package and the chamber walls. From Eq. 1.7,

$$q_{rad} = P_e = \epsilon A_s \sigma (T_s^4 - T_{sur}^4)$$

For the condition when  $T_s = 40^\circ\text{C}$ , with  $A_s = \pi D^2$  the power dissipation will be

$$P_e = 0.25 (\pi \times 0.10^2 \text{ m}^2) \times 5.67 \times 10^{-8} \text{ W/m}^2 \cdot \text{K}^4 \times [(40 + 273)^4 - 77^4] \text{ K}^4 = 4.3 \text{ W} \quad <$$

Repeating this calculation for the range  $40 \leq T_s \leq 85^\circ\text{C}$ , we can obtain the power dissipation as a function of surface temperature for the  $\epsilon = 0.25$  condition. Similarly, with 0.2 or 0.3, the family of curves shown below has been obtained.



**COMMENTS:** (1) As expected, the internal power dissipation increases with increasing emissivity and surface temperature. Because the radiation rate equation is non-linear with respect to temperature, the power dissipation will likewise not be linear with surface temperature.

(2) What is the maximum power dissipation that is possible if the surface temperature is not to exceed  $85^\circ\text{C}$ ? What kind of a coating should be applied to the instrument package in order to approach this limiting condition?